

Nonlinear kinetic inductance in TiN/NbTiN microresonators and Transmission lines

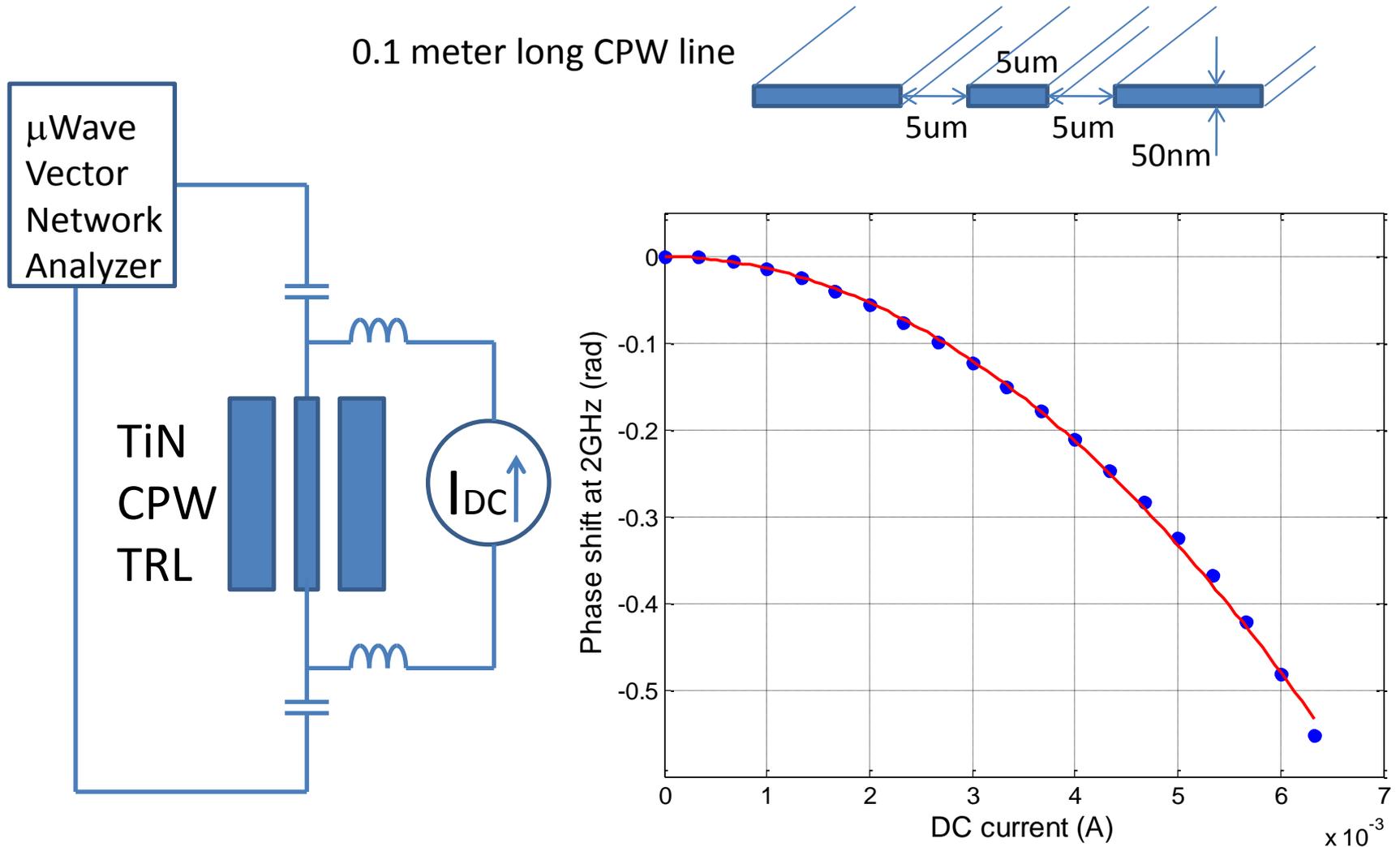
Peter Day

Byeong-Ho Eom

Rick Leduc

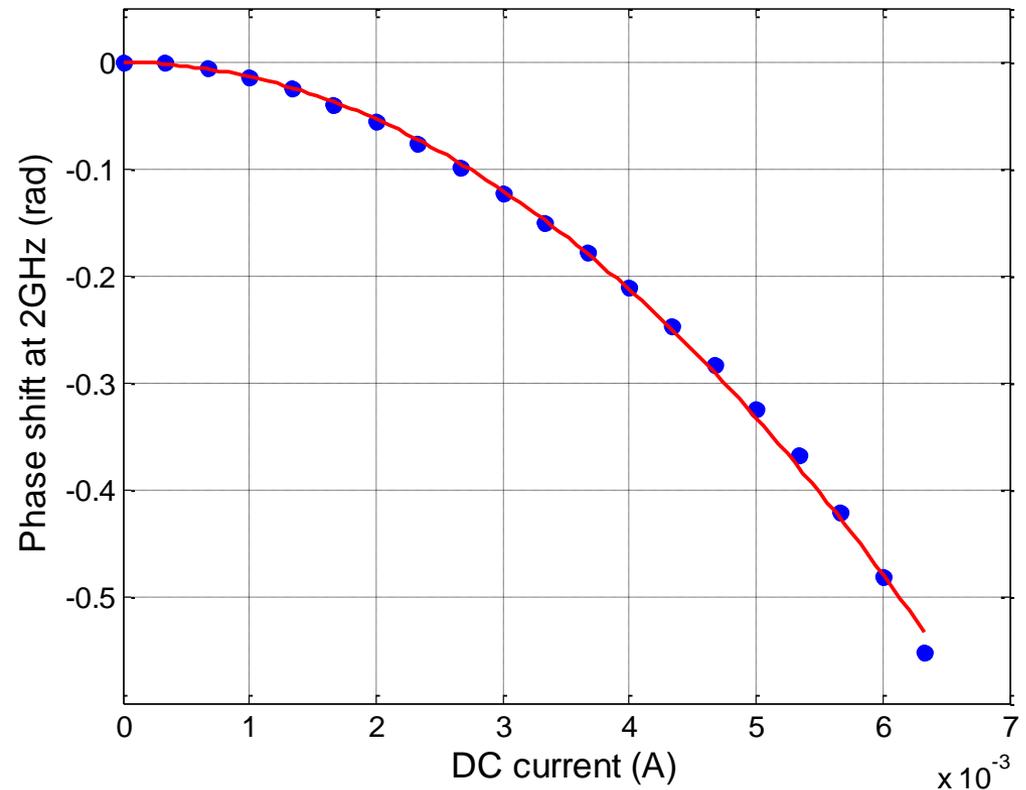
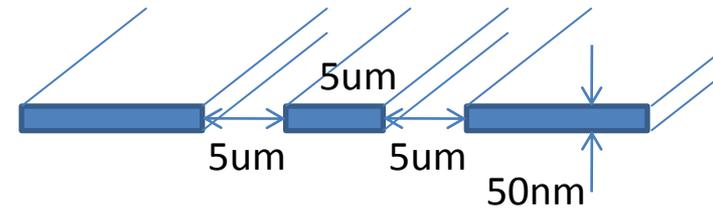
Jonas Zmuidzinas

Nonlinear kinetic inductance



Nonlinear kinetic inductance

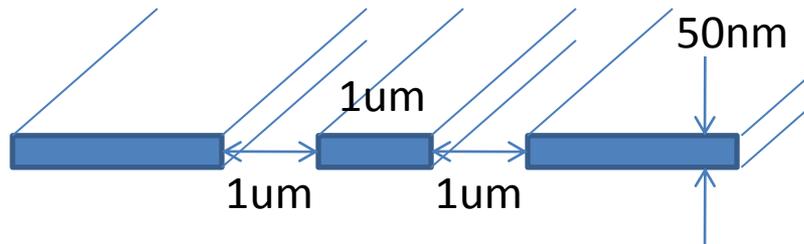
- $\Delta\theta \sim I^2$
- $L = L_0 (1 + I^2/I_*^2)$
- $\delta v_{\text{ph}} \sim I^2 \sim P$
- Kerr medium
- Line length = 0.1m
- > 21 radians
- $\Delta l/l \sim 2.5\%$



Superconducting Nitrides – large kinetic inductance

- $\lambda \approx 105 \text{ nm} \times (\rho_n [\mu\Omega.\text{cm}] / T_c [\text{K}])^{1/2}$
 - Nitrides: $\rho_s \approx 100 \mu\Omega.\text{cm}$
 - λ (TiN, NbTiN) $\approx 500 \text{ nm}$

Example: TiN CPW line



$$L_s / L_{\text{tot}} \approx 0.94$$

$$v_{\text{ph}} \approx 0.1 c$$

$$Z_0 \approx 220 \Omega$$

Kinetic Inductance Non-linearity

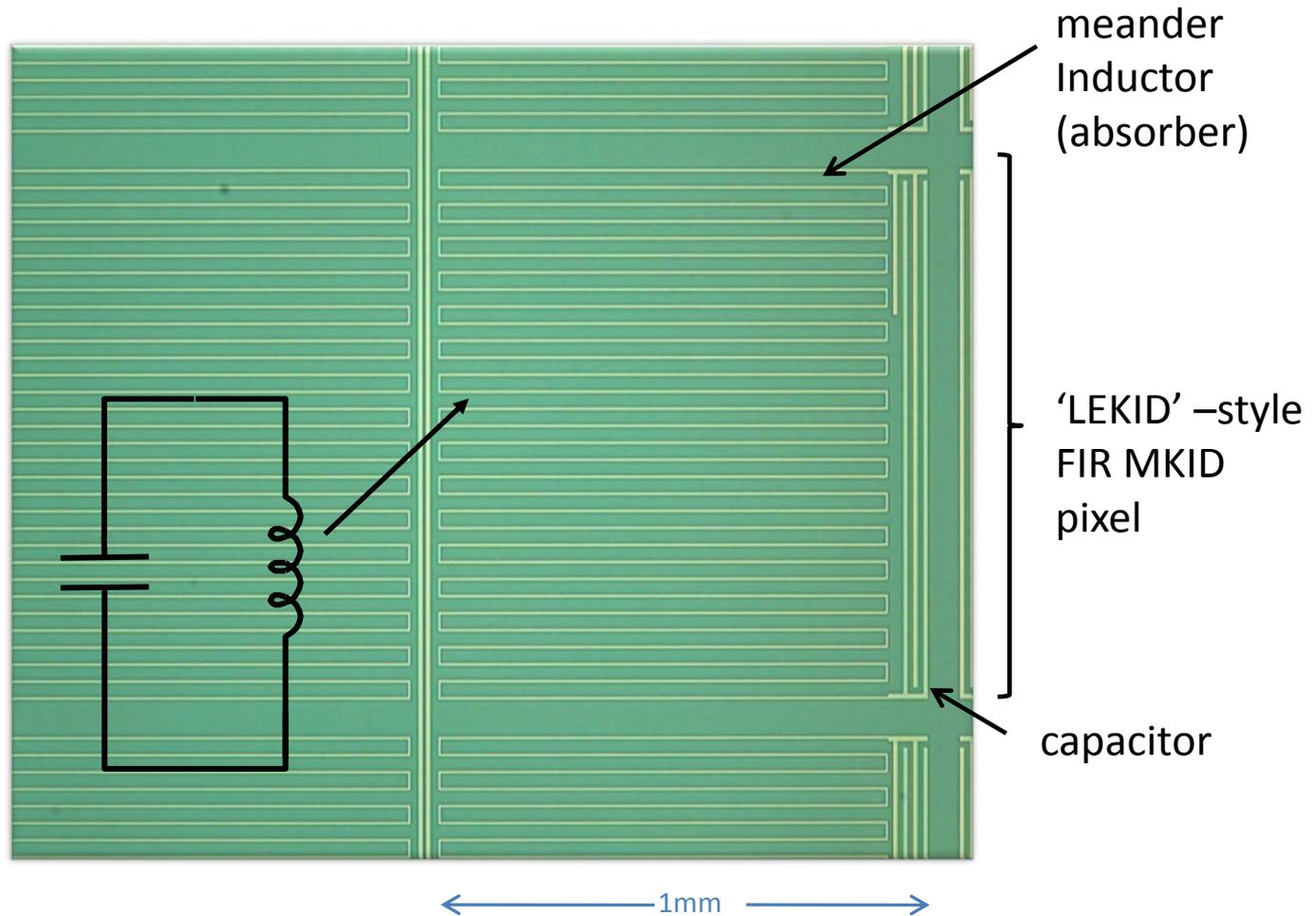
- Ginsberg-Landau theory
 - $L_s(I)$, $\lambda(I)$

$$\frac{\delta v_{\text{ph}}}{v_{\text{ph}}(I=0)} = \frac{-L_{\text{kin}}}{4 L_{\text{tot}}} \frac{\mu_0 \lambda^2 J_s^2}{\mu_0 H_c^2}$$

Supercurrent kinetic energy

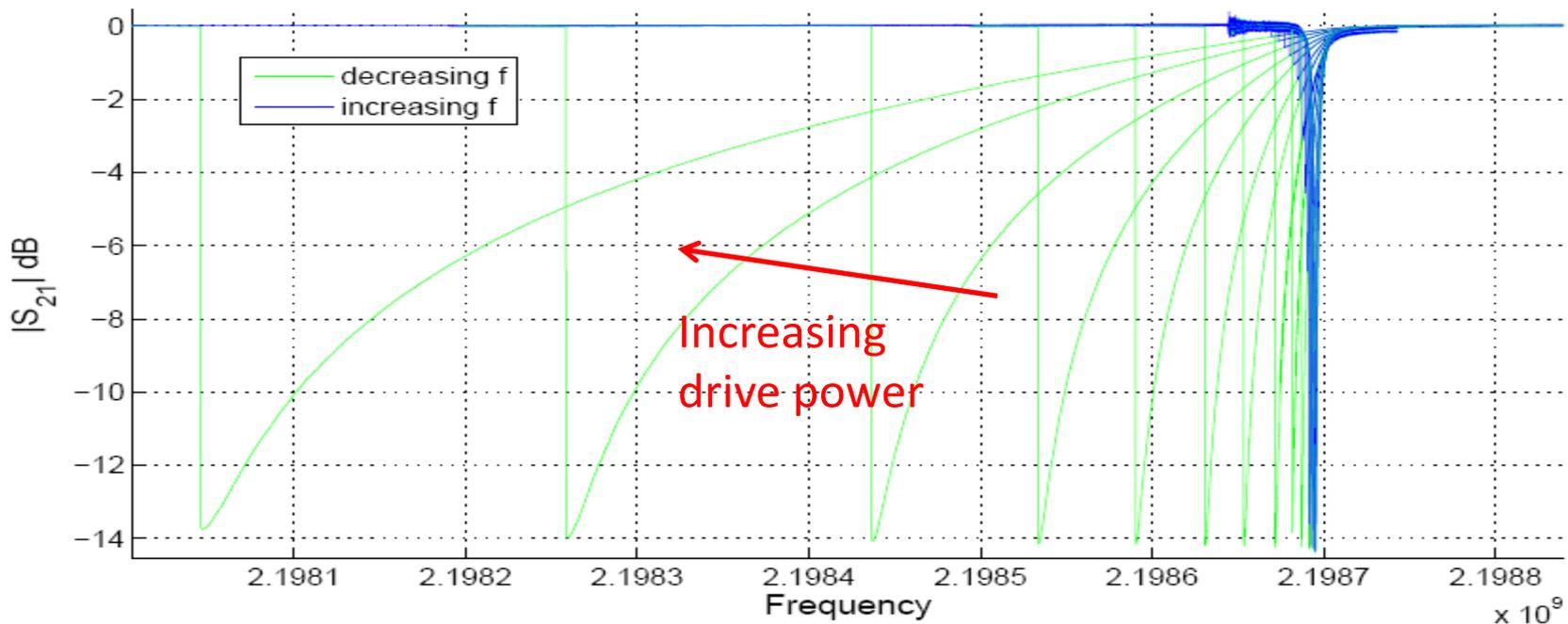
Condensation energy

TiN Resonator measurements

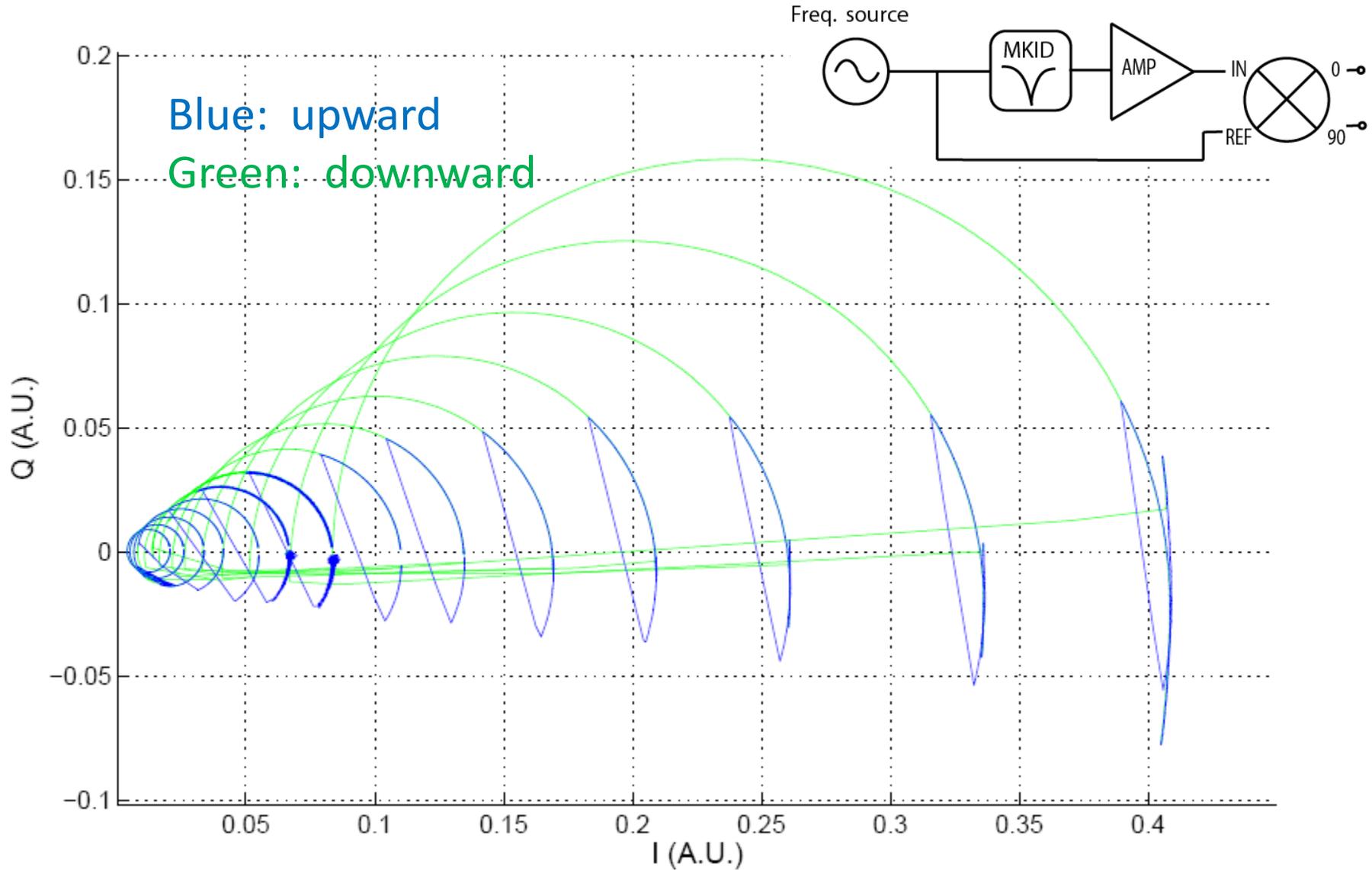


Nonlinear “Duffing” oscillator

- Resonance frequency depends on resonator current
- Hysteretic resonance curves:



Complex transmission



Non-linear resonator model

$$\delta f/f_0 = -k_f I_{res}^2$$

$$\delta Q_i^{-1} = k_Q I_{res}^2$$

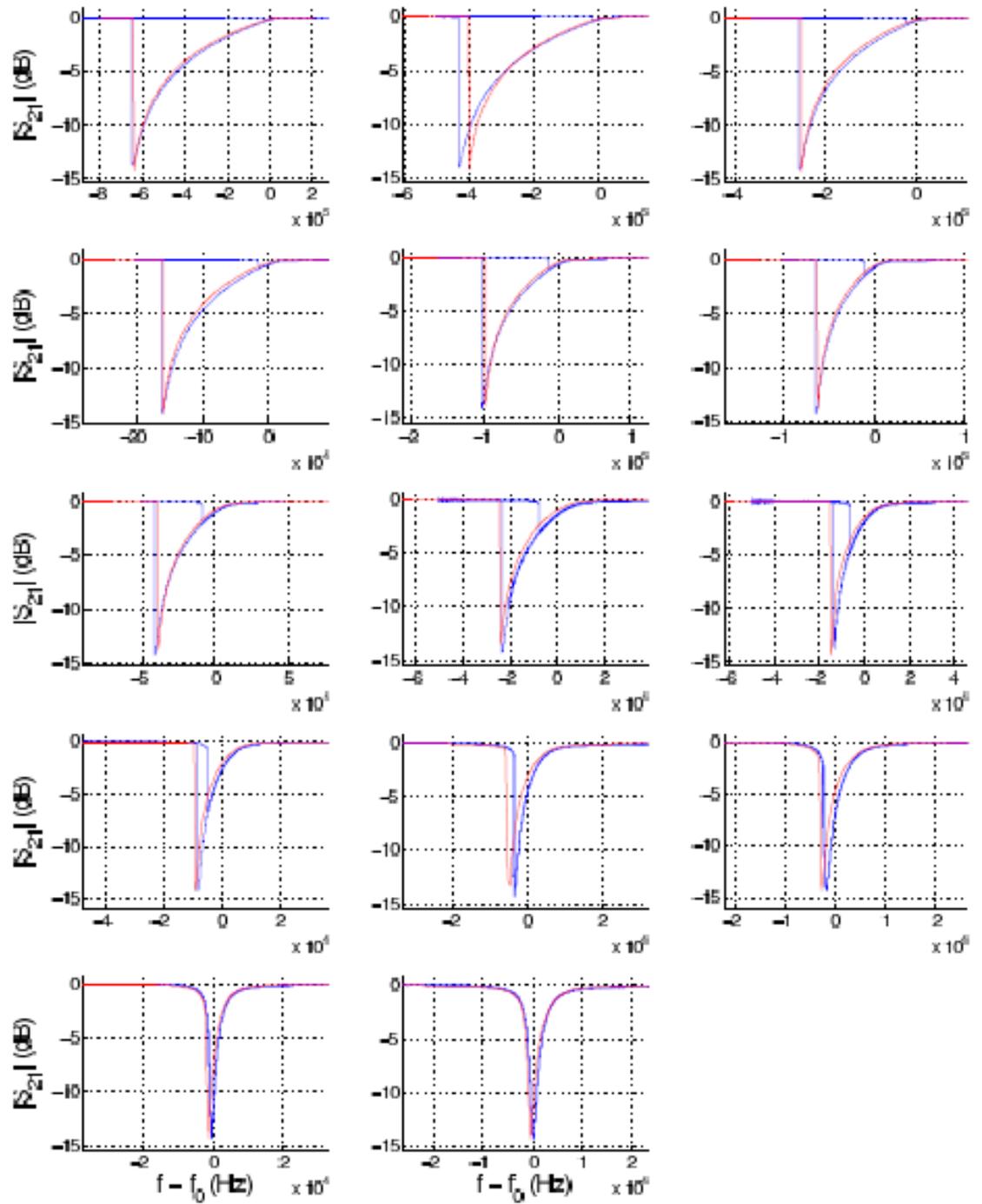
See Yurke and Buks (2008);
Dahm and Scalapino (1997)

$$S_{21} = 1 - \frac{Q_t/Q_c}{1 + 2iQ_t[f_0 + \delta f_0(f) - f]/f_0}$$

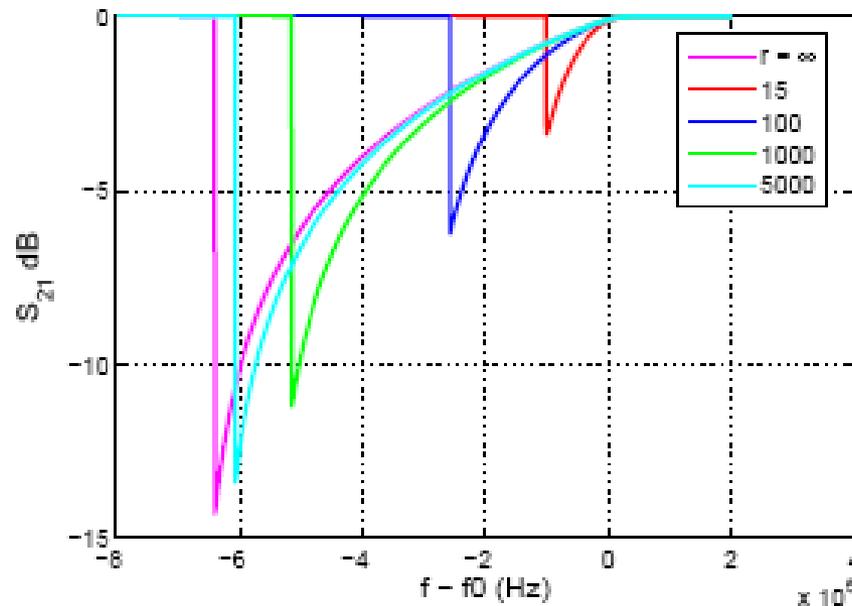
$$\frac{1}{Q_t} = \frac{1}{Q_c} + \frac{1}{Q_i}$$

$$I_{res}^2 = \frac{Q_c |1 - S_{21}|^2 P_{feedline}}{Z_0}$$

- Fits using NL resonator model
- $K_Q = 0$!

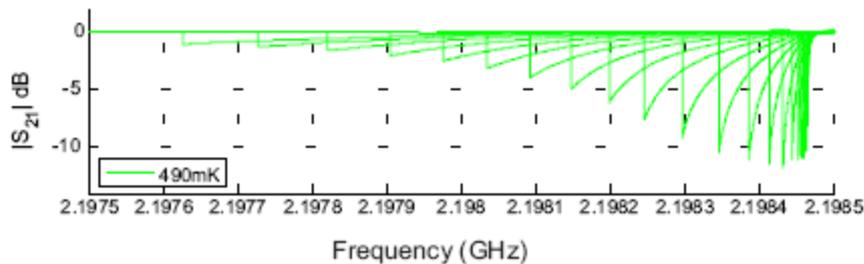
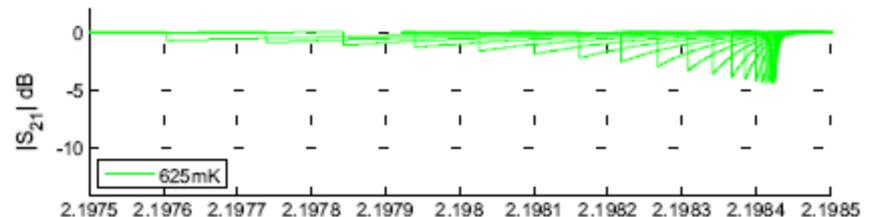
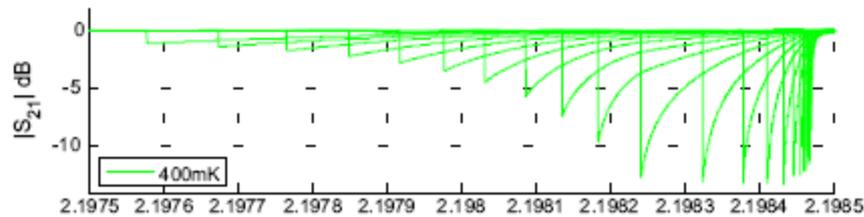
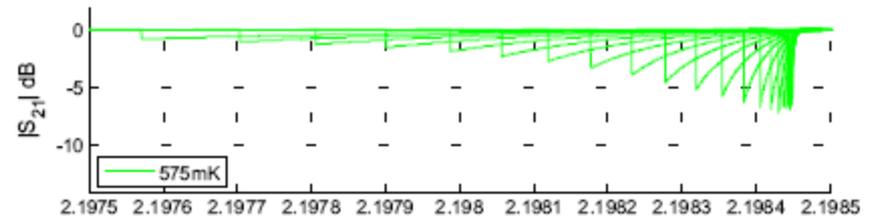
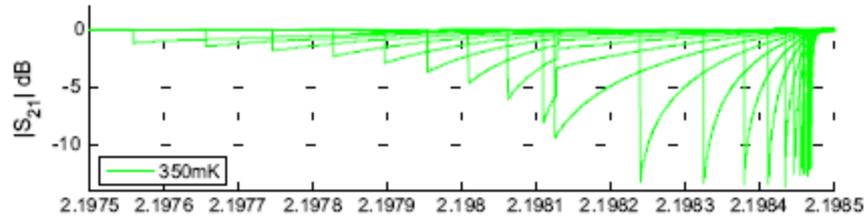
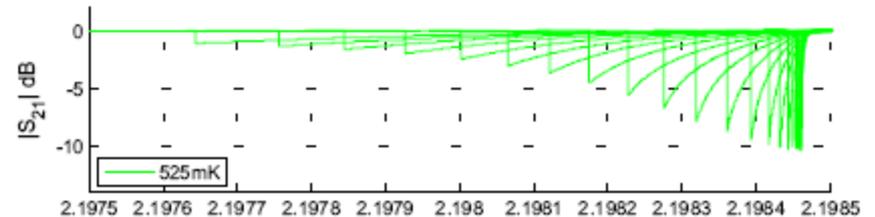
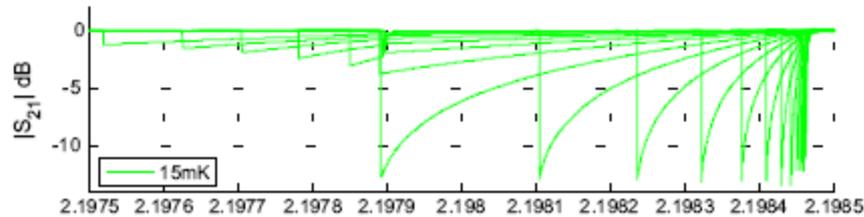


- Model results for different ratios of inductive to dissipative response



- $\delta \text{ resistance} / \delta \text{ reactance} < 2 \times 10^{-4}$

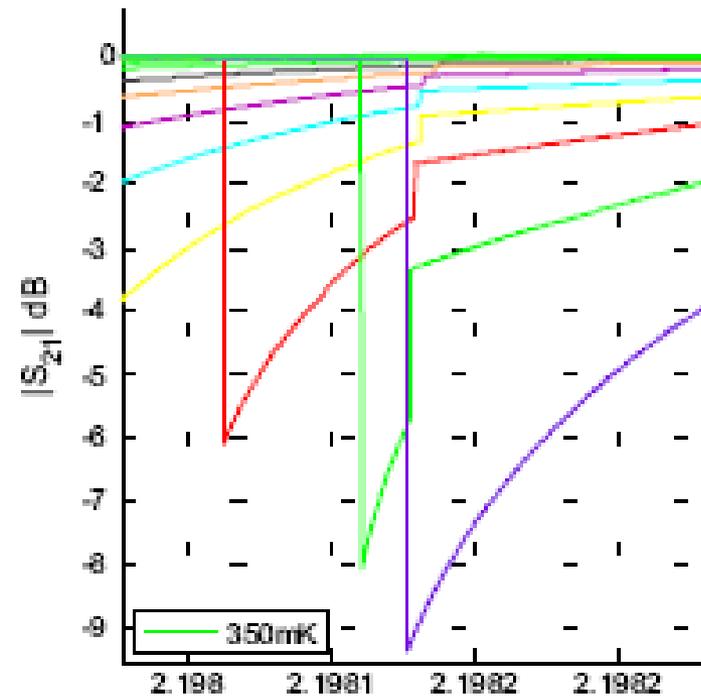
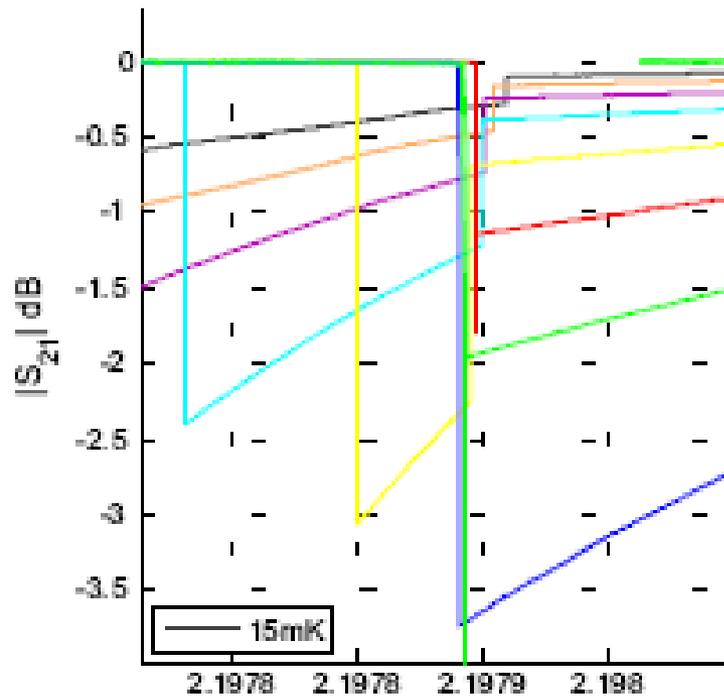
Measurements at elevated T

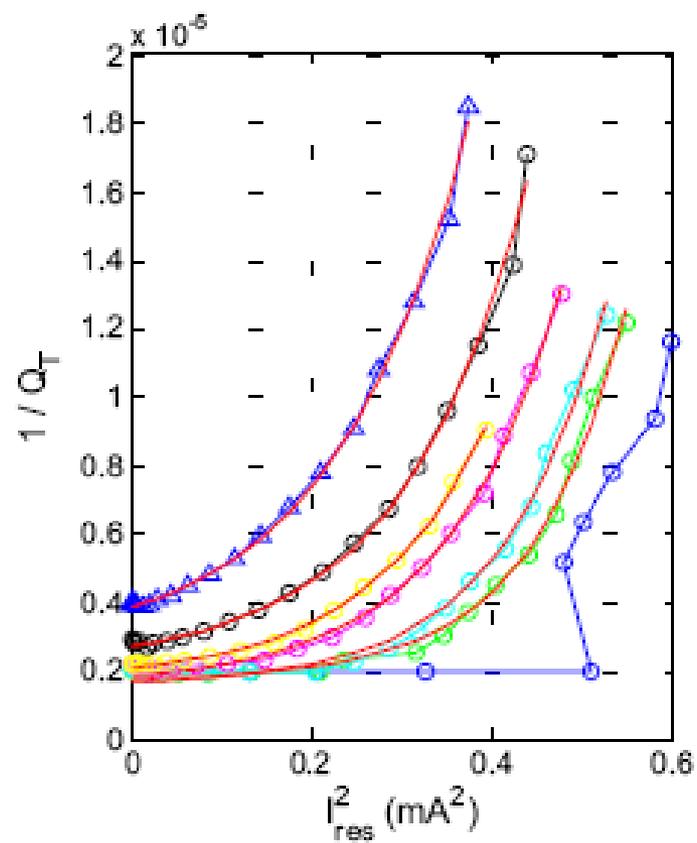
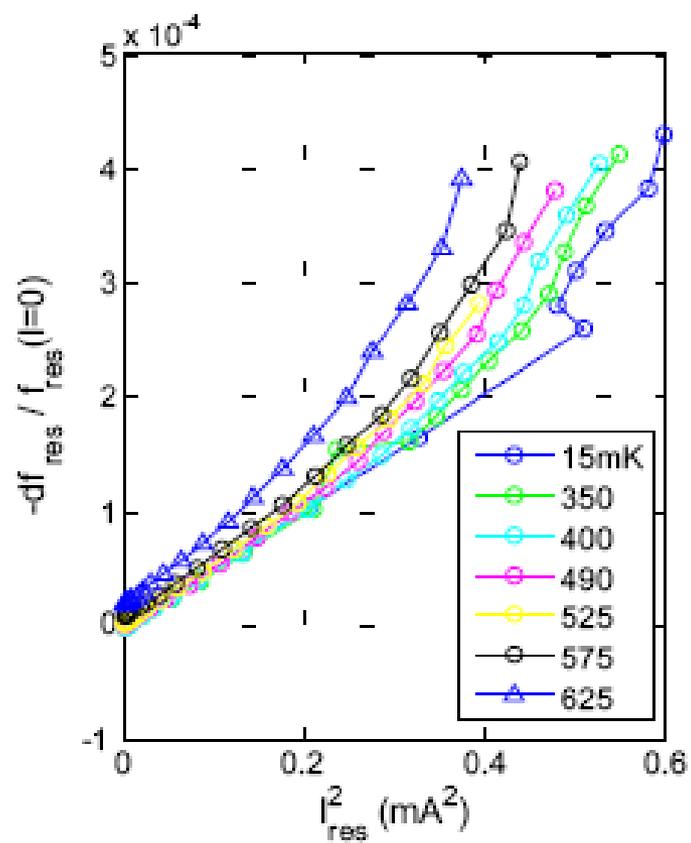


Frequency (Ghz)

Frequency (GHz)

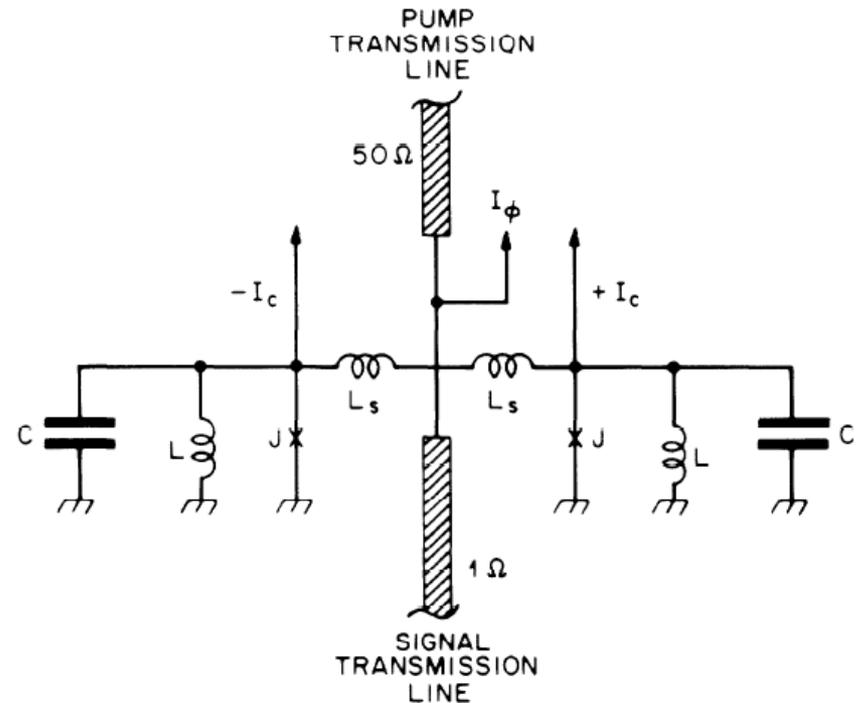
Transition to dissipative regime





Josephson parametric amplifiers

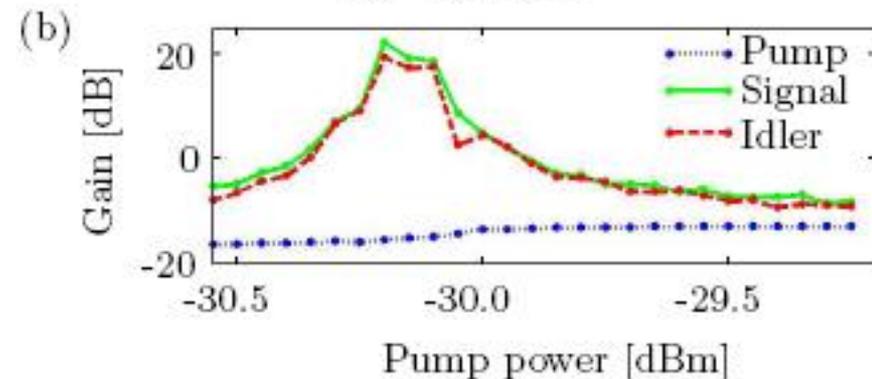
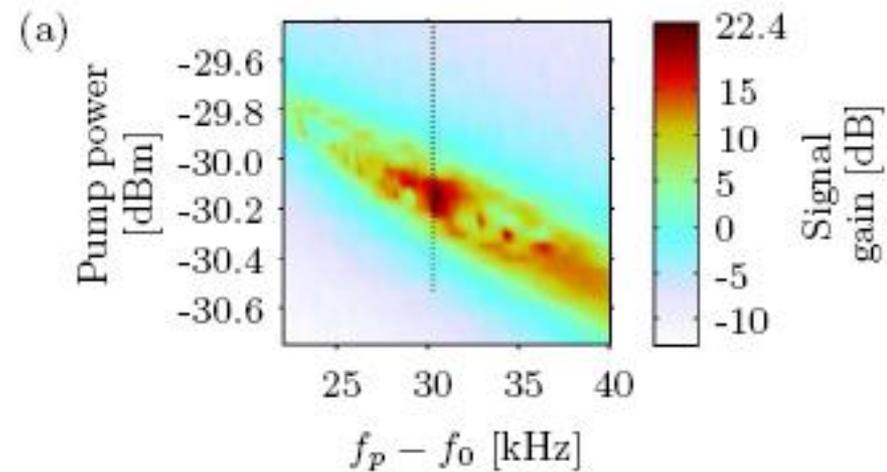
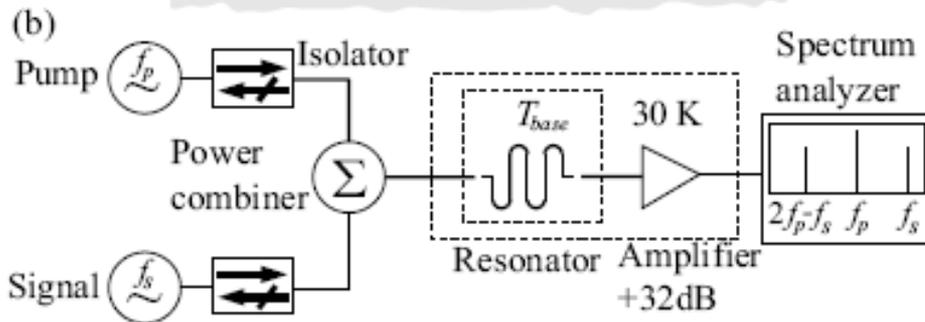
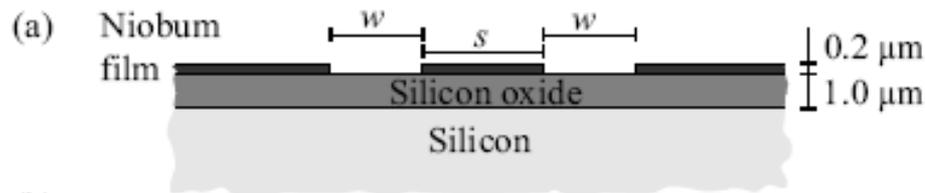
- Nonlinearity
 - Josephson inductance
 - Transfer of energy from strong pump to signal
 - Idler tone
- Purely reactive nonlinearity
 - May reach QL
- Resonant, narrow band



Yurke et al. (1988)

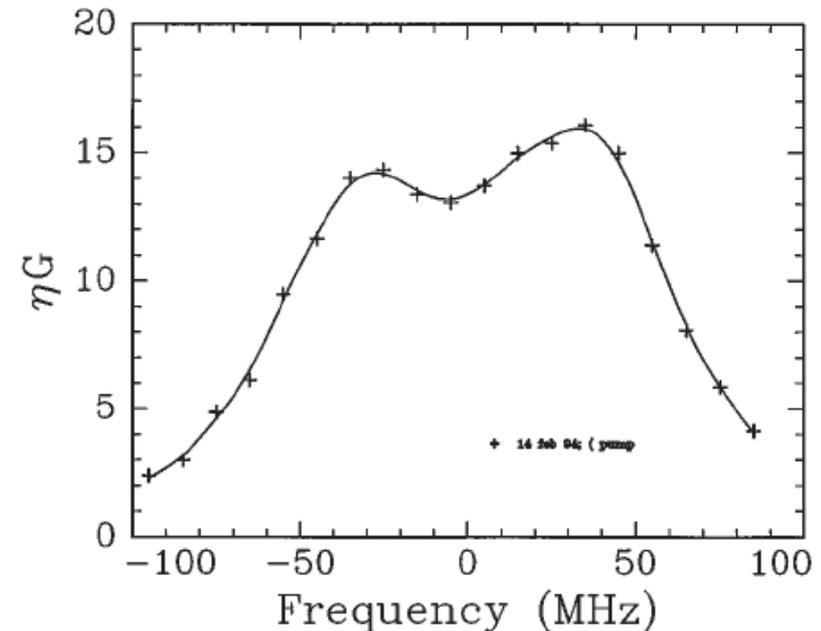
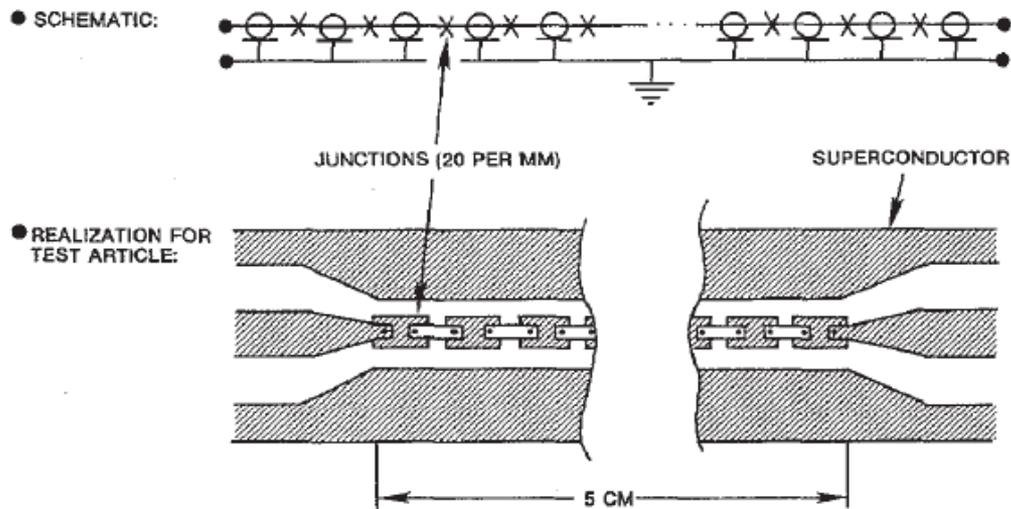
Kinetic inductance cavity para-amp

- Tholen et al. (2007)
- Nb CPW resonator



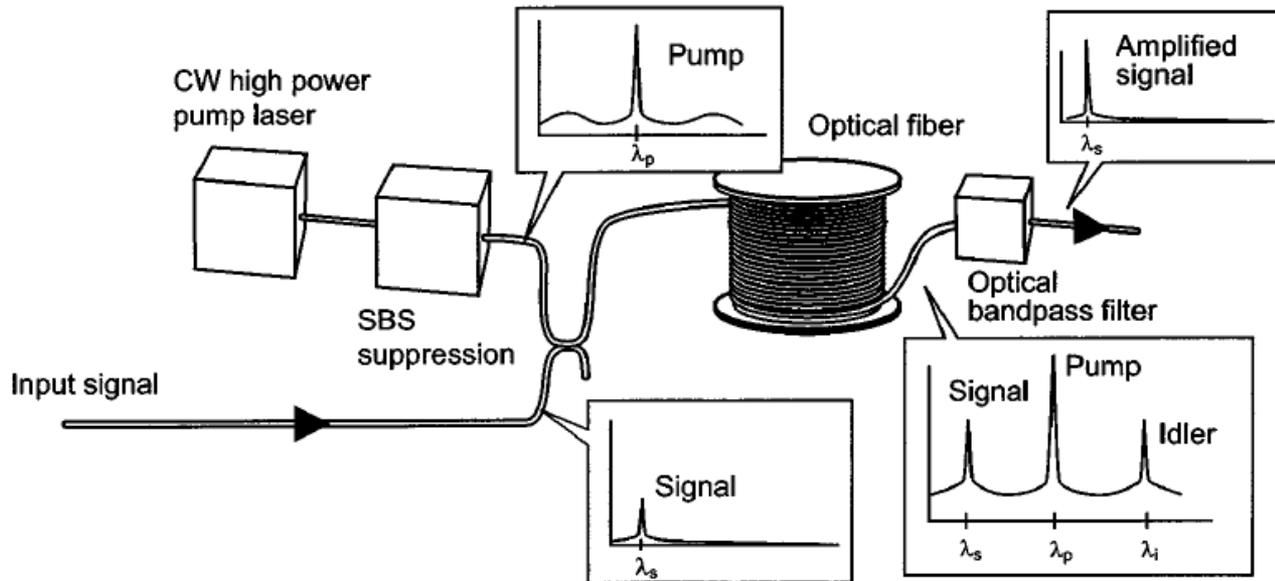
Traveling wave Josephson paramp

- Proposed by Sweeny and Mahler (1985)
- Experimentally realized by Yurke et al. (1996)
- Gain x bandwidth $\sim 500\text{MHz}$



Optical fiber paramp

- Intensity dependent index: $n \sim E^2$
- Kerr medium

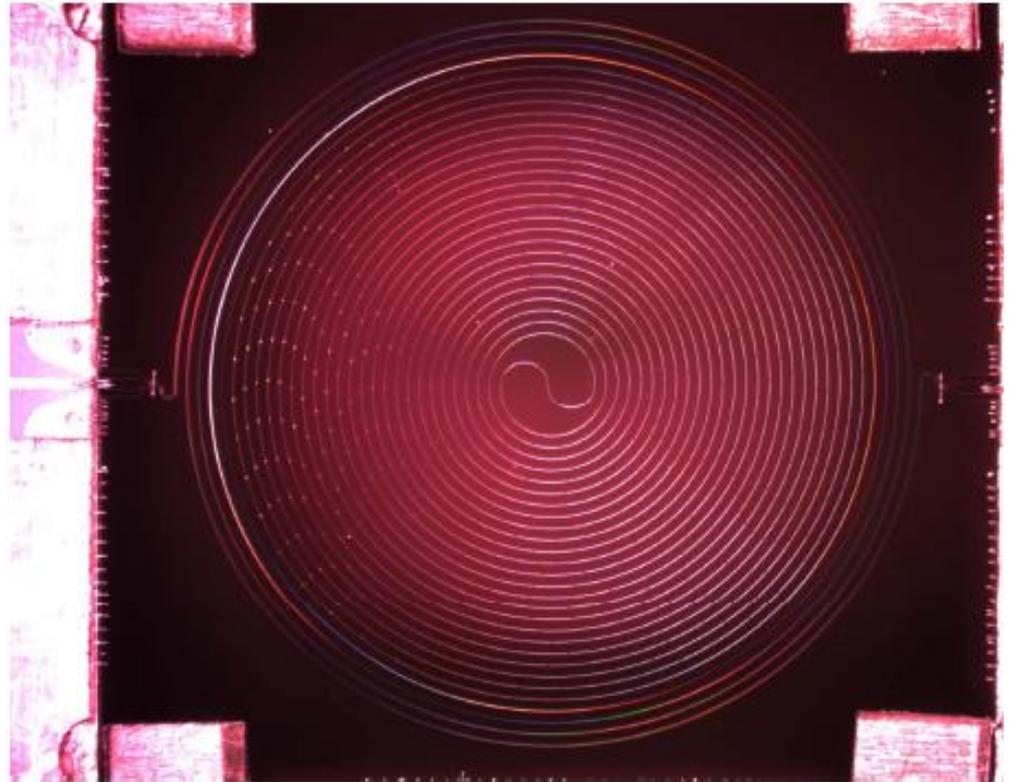
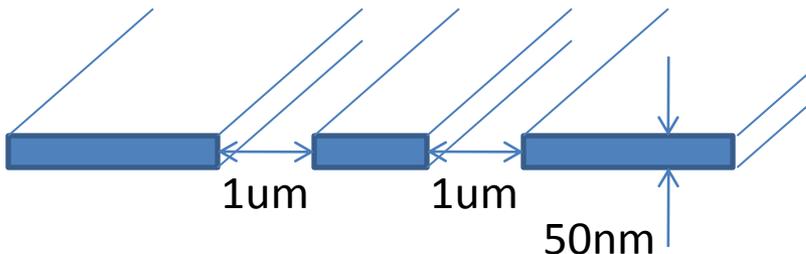


from Hansryd
et al. (2002)

- Yurke's device an analogue of this

DTWKI paramp ver 1.0

- DTWKI = Dispersion-engineered Traveling Wave Kinetic Inductance
- Single layer TiN or NbTiN
- 0.8 m CPW line
 - Tapers at input, output match 50 ohms



Coupled mode equations

- From the optical fiber paramp: (Stohlen et al.)

$$\begin{aligned} \frac{dA_p}{dz} &= i\gamma[(|A_p|^2 + 2(|A_s|^2 + |A_i|^2))A_p \\ &\quad + 2A_s A_i A_p^* \exp(i\Delta\beta z)], \\ \frac{dA_s}{dz} &= i\gamma[(|A_s|^2 + 2(|A_i|^2 + |A_p|^2))A_s \leftarrow \text{SPM, XPM} \\ &\quad + A_i^* A_p^2 \exp(-i\Delta\beta z)], \leftarrow \text{Energy transfer} \\ \frac{dA_i}{dz} &= i\gamma[(|A_i|^2 + 2(|A_s|^2 + |A_p|^2))A_i \\ &\quad + A_s^* A_p^2 \exp(-i\Delta\beta z)]. \end{aligned}$$

- $A_{p,s,i}$: slowly varying (complex) amplitudes
- γ : non-linearity parameter
- $\Delta\beta = \beta(\omega_s) + \beta(\omega_i) - 2\beta(\omega_p)$

Coupled mode equations

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Without dispersion ($\Delta\beta = 0$):

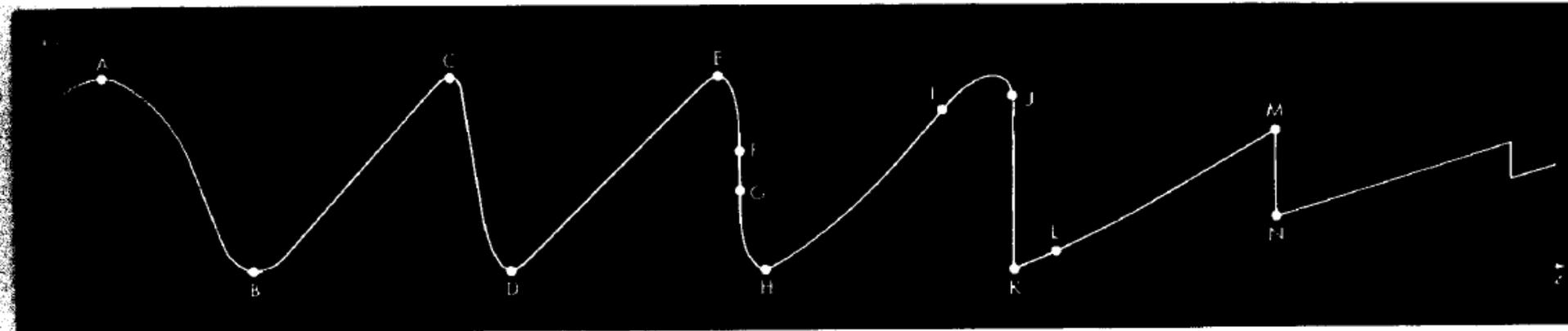
$$G = 1 + (\gamma P_p L)^2 = 1 + (\Delta\theta)^2$$

Total phase shift in radians
in response to pump

Shock wave formation

- Superconducting TRLs are virtually dispersionless
- Harmonic generation is efficient

Figure 3 Voltage as a function of distance along the line, due to a periodic voltage applied at $z=0$. *FG* is a shock wave that has just formed. The shock wave *JL* is near its maximum amplitude. *MN* is a shock wave decreasing in amplitude.



Landauer (1960)

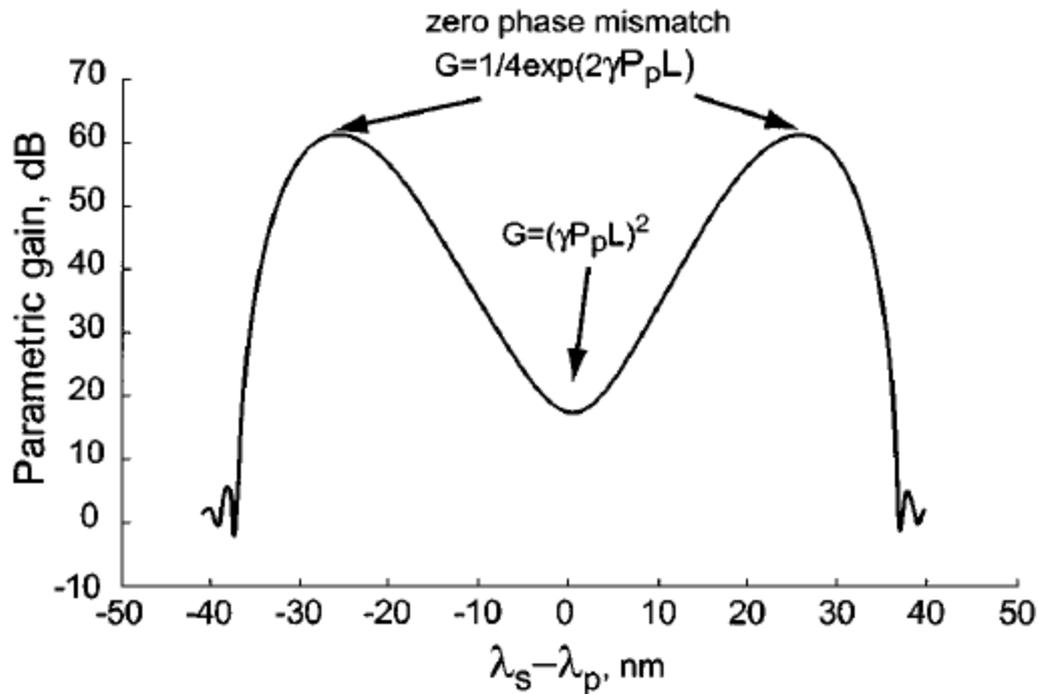
$$L = L_0(1 + I^2/I_*^2)$$

$$V = LdI/dt$$

$$I^2dI/dt \longrightarrow 3f_P \longrightarrow 5f_P, 7f_P, \text{ etc.}$$

Adding dispersion

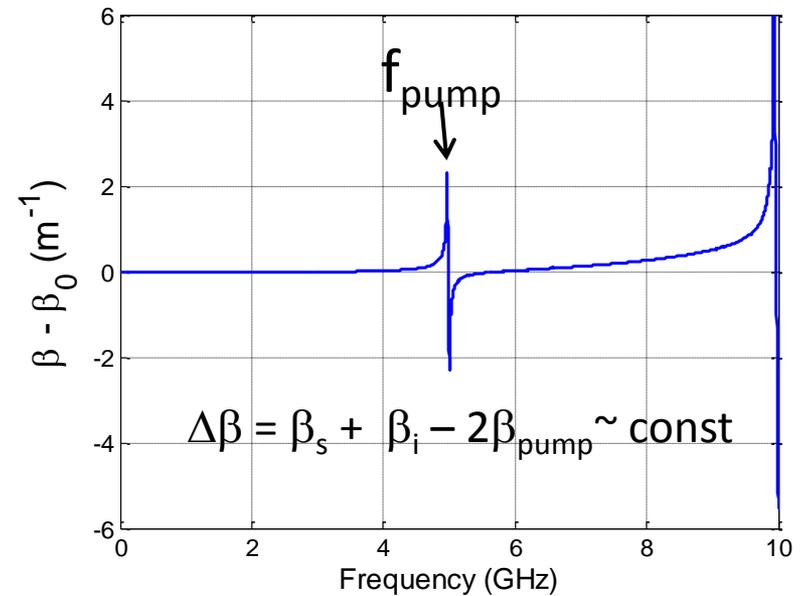
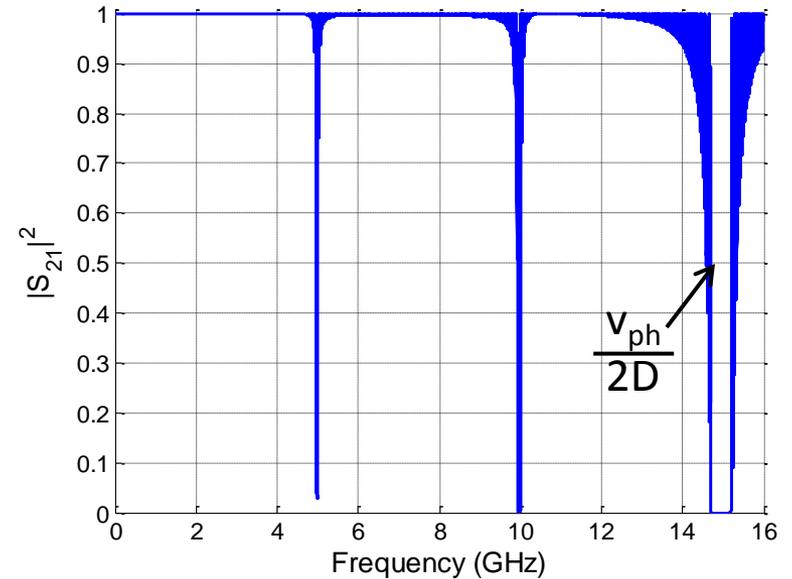
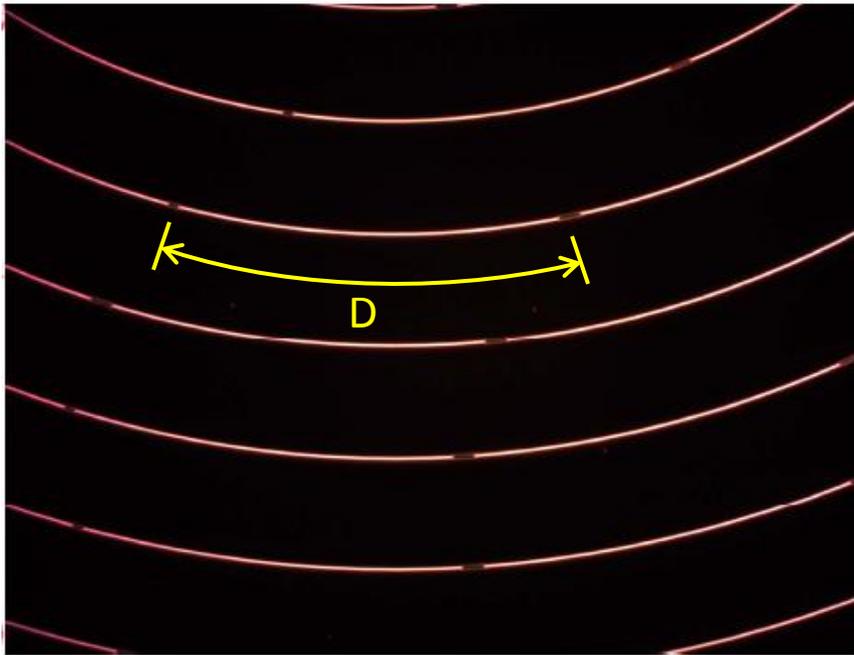
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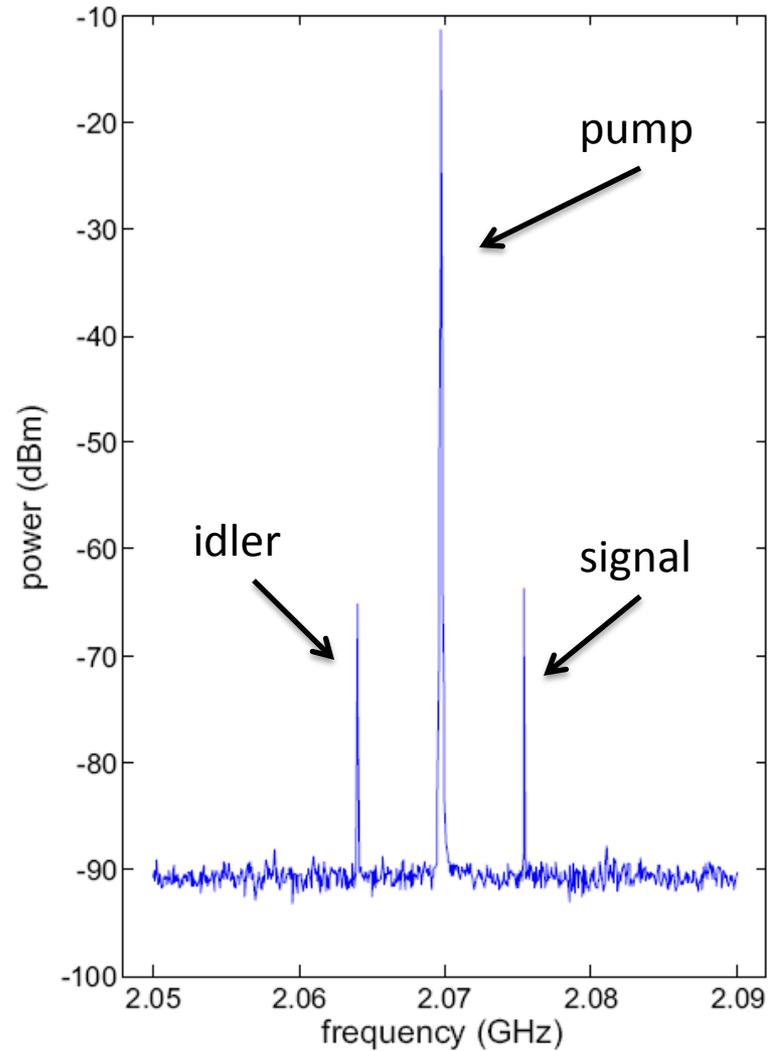
- Phase mismatch
 - Limited bandwidth
- Optimal dispersion compensates nonlinear phase mismatch
 - Exponential gain regime

Dispersion-engineered traveling wave kinetic inductance (DTWKI) amplifier

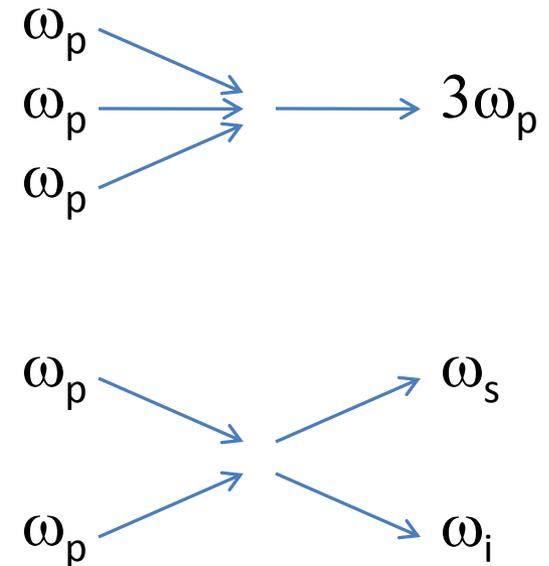
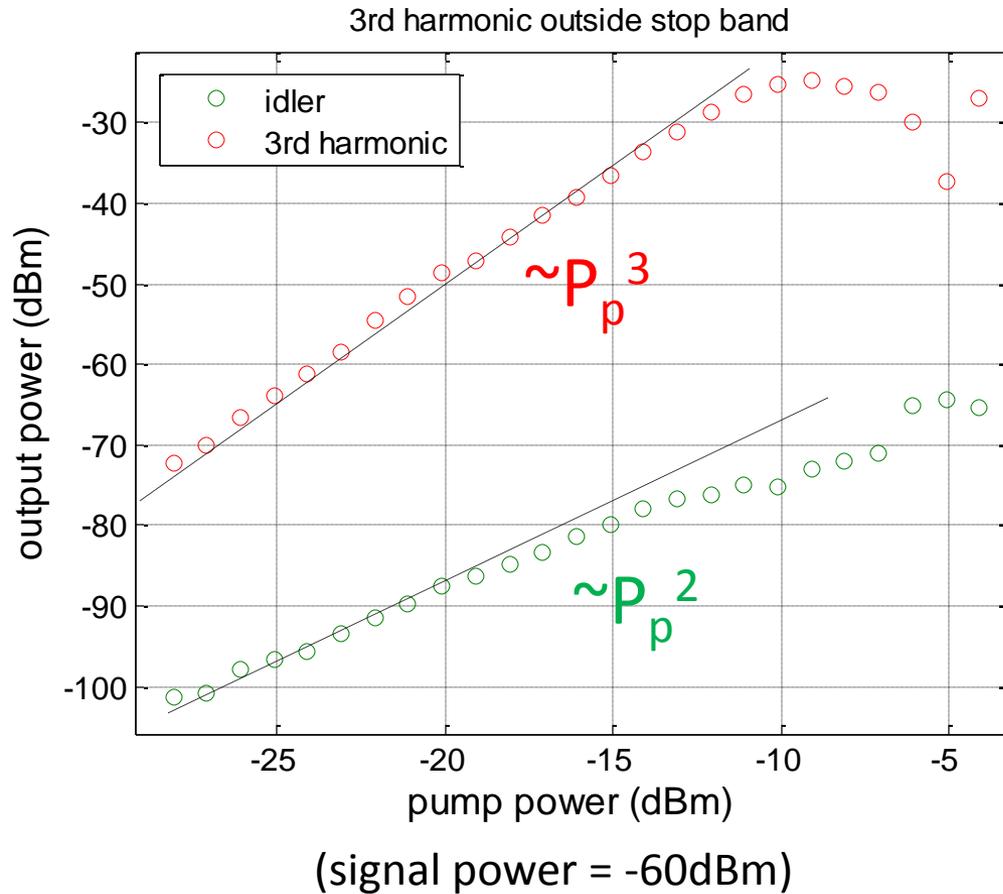
- Periodically load TRL
 - Produce stop band at $3 \times f_{\text{pump}}$
 - Dispersion around f_{pump}



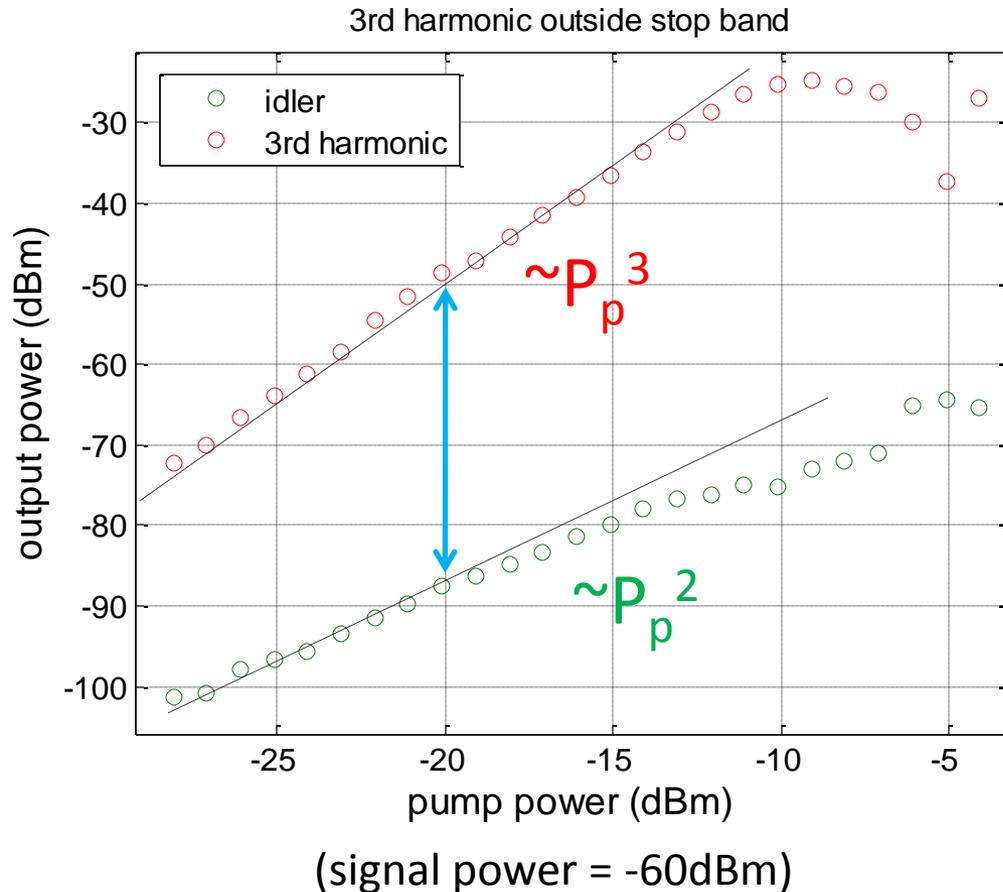
Idler generation



3rd Harmonic/Idler Generation



3rd Harmonic/Idler Generation



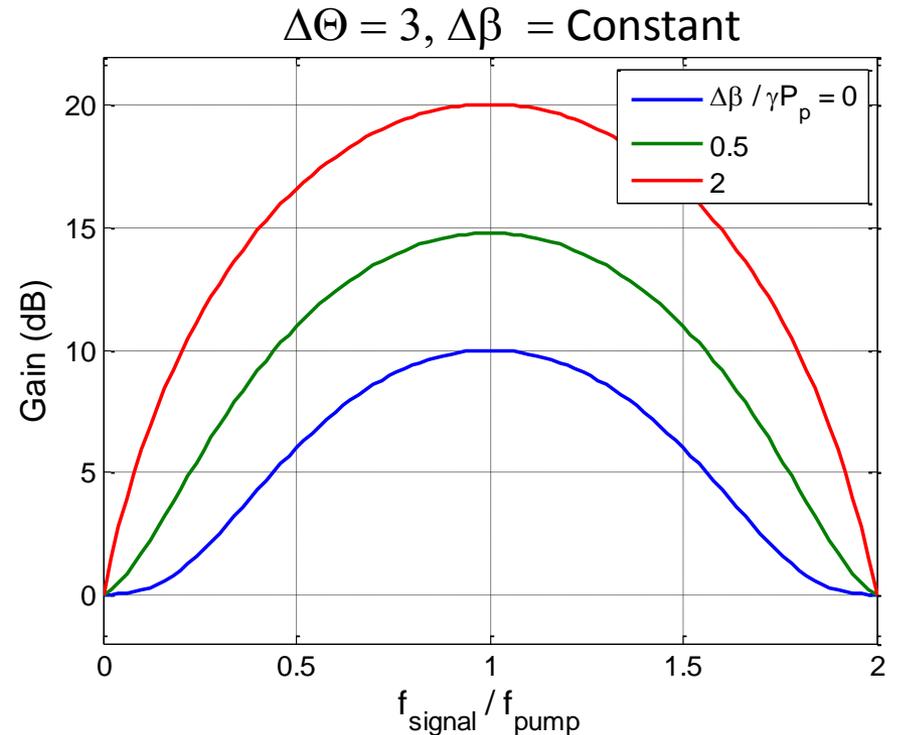
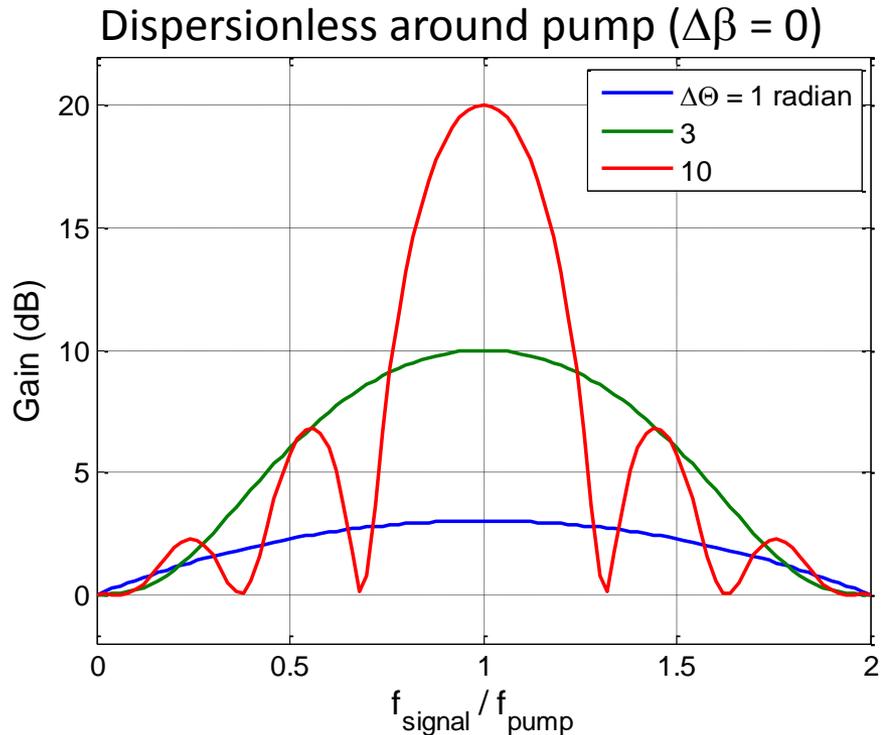
$$\frac{P_{\text{out}}(3\omega_p)}{P_{\text{out}}(\omega_i)} = \frac{P_p}{P_s}$$

eg. @ $P_p = -20$ dBm,
 $P_s = -60$ dBm

$$\frac{P_{\text{out}}(3\omega_p)}{P_{\text{out}}(\omega_i)} = 40 \text{ dB}$$

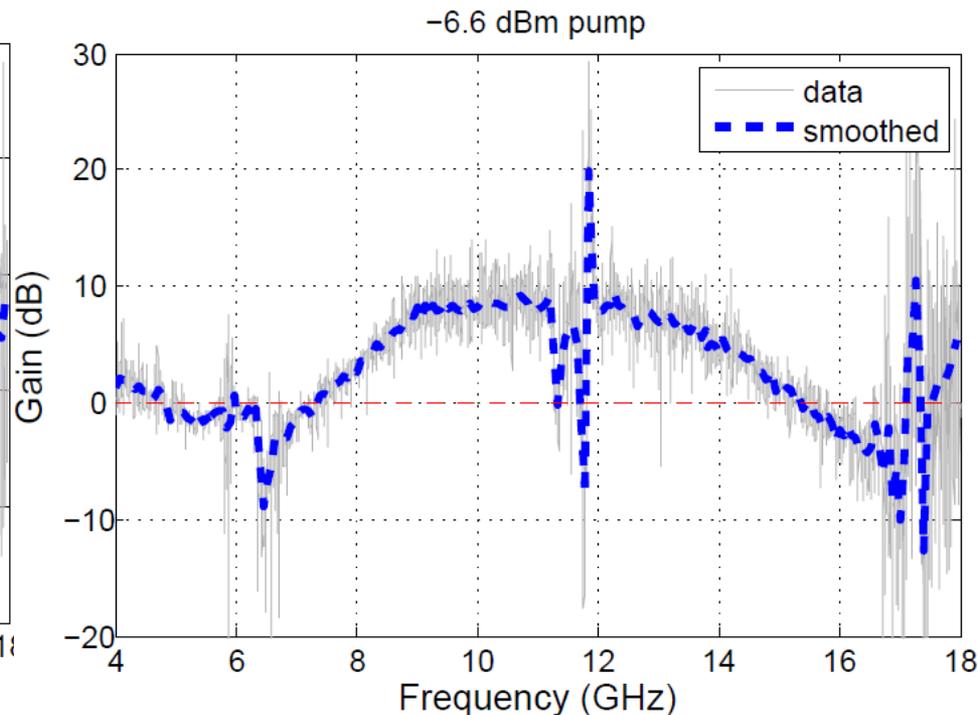
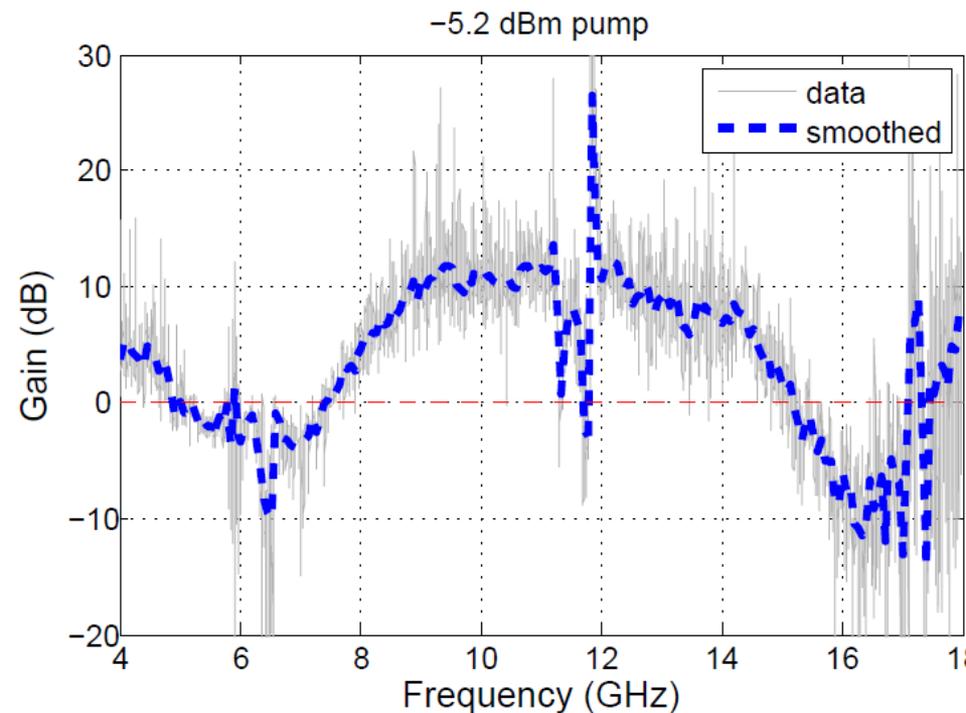
Coupled-mode prediction

- Assume harmonic generation blocked



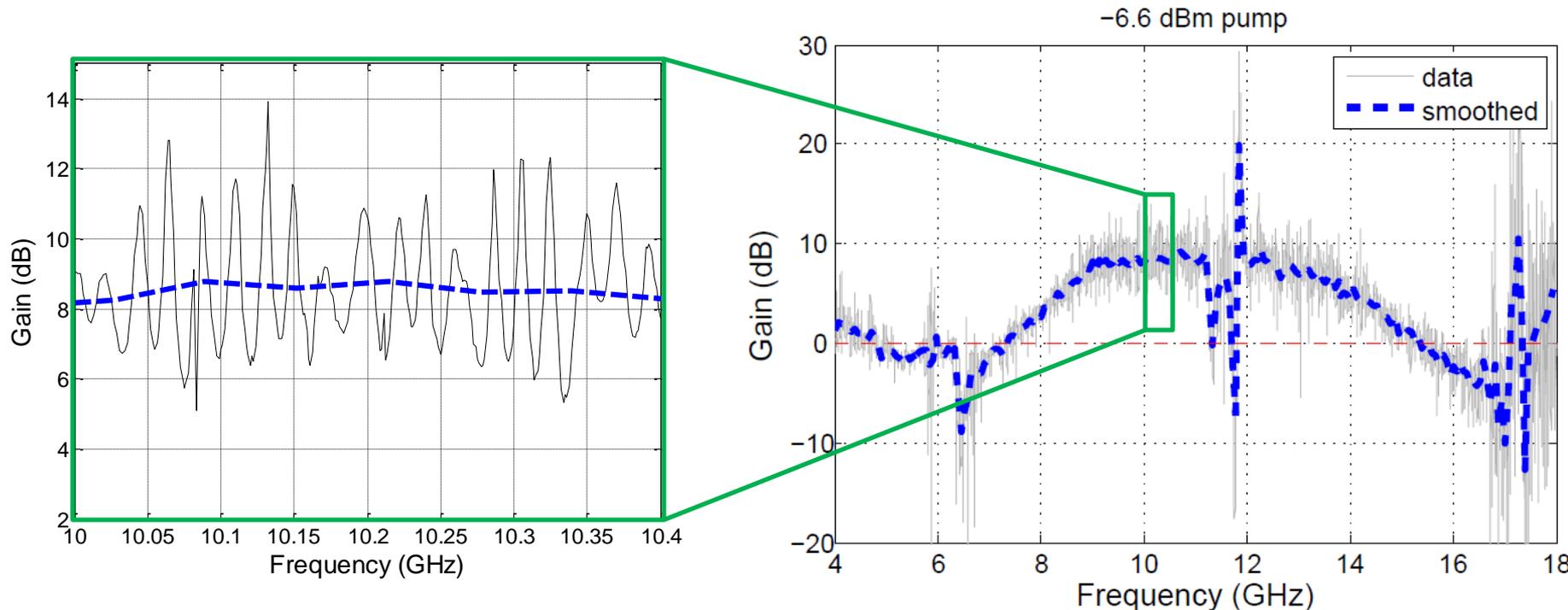
Paramp gain

- NbTiN device, pump at 11.56 GHz
 - Near (2nd) engineered dispersion feature



Paramp gain

- NbTiN device, pump at 11.56 GHz
 - Near (2nd) engineered dispersion feature
- Ripple due to reflections, amplifying medium



Conclusion

- Nonlinearity, low dissipation of superconducting nitride films enables a new broad-band paramp
- Measured gain roughly consistent with expectations
 - Noise measurements are underway
- Applications
 - Microwave amp for detector array readout
 - Potential of QL performance
 - Radio astronomy (mm – submm)
 - NbTiN gap frequency > 1 THz
 - Quantum information
 - Axion search